

Compressive sensing meets time-frequency: An overview of recent advances in time-frequency processing of sparse signals

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Abstract

Compressive sensing is a framework for acquiring sparse signals at sub-Nyquist rates. Once compressively acquired, many signals need to be processed using advanced techniques such as time-frequency representations. Hence, we overview recent advances dealing with time-frequency processing of sparse signals acquired using compressive sensing approaches. The paper is geared towards signal processing practitioners and we emphasize practical aspects of these algorithms. First, we briefly review the idea of compressive sensing. Second, we review two major approaches for compressive sensing in the time-frequency domain. Thirdly, compressive sensing based time-frequency representations are reviewed followed by descriptions of compressive sensing approaches based on the polynomial Fourier transform and the short-time Fourier transform. Lastly, we provide brief conclusions along with several future directions for this field.

Keywords:

Compressive sensing, time-frequency analysis, time-frequency dictionary, nonstationary signals, sparse signals

1. Introduction

Time-frequency analysis provides a framework for a descriptive analysis of non-stationary signals whose models are not available or easily constructed [1], [2]. For such signals, time or frequency domain descriptions typically do not offer comprehensive details about changes in signal characteristics [3]. The main issue with the time domain representation is that it provides no details about the frequency content of those signals, and sometimes, even the time content can be difficult to interpret [4]. The frequency domain on

8 the other hand provides no easily understood timing details about the occurrence of vari-
9 ous frequency components [5]. In other words, timing details are buried within the phase
10 spectrum of a signal, which is the most common reason for only analyzing the amplitude
11 spectrum of a signal obtained via the Fourier transform. To combine timing and spectral
12 into a joint representation, a time variable is typically introduced into a Fourier-based
13 analysis to obtain two-dimensional, redundant representations of non-stationary signals
14 [6]. Such representation provide a description of spectral signal changes as a function
15 of time, that is, the description of time-varying energy concentration changes along the
16 frequency axis. In an ideal case, these two-dimensional signal representations would com-
17 bine instantenous frequency spectrum with global temporal behavior of a signal [7], [8],
18 [9],[10], [11], [12], [13], [14], [15].

19 Time-frequency analysis is often employed in the analysis of complex non-stationary
20 signals (e.g., physiological signals [16], [17], [18], [19], [20], [21], [22], [23], mechanical
21 vibrations [24], [25], [26], [27], audio signals [28], [29], [30], radar signals [31], [32], [33],
22 [34], [35], [36]). However, continuously monitoring such signals for an extended period
23 of time can impose heavy burdens on data acquisition and processing systems, even
24 when sampling these non-stationary signals at low sampling rates. To avoid these data
25 acquisition and processing burdens, compressive sensing aims to compress signals during
26 a data acquisition process, rather than afterwards [37], [38], [39], [40], [41], [42], [43], [44],
27 [45], [46], [47], [48], [49], [50], [51], [52].

28 In this paper, we review recent advances that combine the ideas of time-frequency
29 and compressive sensing analyses. Section 2 reviews the main ideas behind compres-
30 sive sensing. In Section 3, we introduce the main approaches to obtain compressed
31 samples in the time-frequency domain. Several different approaches are presented here
32 including compressive sensing in the ambiguity domain, but also compressive sensing of
33 non-stationary signals using time-frequency dictionaries. We also reviewed compressive
34 sensing approaches that relied on the short-time Fourier transform and the polynomial
35 Fourier transform. Compressive sensing based time-frequency representations are de-
36 scribed in Section 4. Conclusions and future directions are provided in Section 5.

37 2. Compressive Sensing

38 In traditional signal processing, the Shannon-Nyquist sampling theorem mandates
39 that any signal needs to be sampled at least twice the highest frequency present in the
40 signal to be able to accurately recover information present in the signal. The traditional
41 sampling approach can yield a large number of samples, and compressive strategies are
42 often used immediately after sampling in order to reduce storage requirements or trans-
43 mission complexities. While this has been a prevailing approach for many years, it is
44 clearly a redundant approach as most of acquired samples are disregarded immediately
45 after sampling. To avoid these redundant steps, compressive sensing has been proposed
46 and it postulates a signal can be recovered using a fewer number of samples than required
47 by the Shannon-Nyquist theorem [38], [39], [53], [40], [54] [55], [56], [57], [58], [59], [60],
48 [61], [62], [63].

49 The main idea behind compressive sensing is to combine sensing and compression steps
50 into a single step during a data acquisition process [39], [40], [42], [64], [65]. Compressive
51 sensing approaches typically acquire signals at sub-Nyquist rates (e.g., one tenth of the
52 Nyquist rate) and signals can be accurately recovered from these samples with *a certain*
53 *probability* [39]. These approaches work very well for K -sparse signals, i.e., signals that
54 can be represented by K bases in an N -dimensional space. In other words, compressive
55 sensing approaches will acquire $M \ll N$ samples that will encode a K -sparse signal of
56 dimension N by computing a measurement vector \mathbf{y} of a signal vector \mathbf{s} [66], [67], [68],
57 [69]:

$$\mathbf{y} = \Phi \mathbf{s} \tag{1}$$

58 where Φ represents an $M \times N$ sensing matrix [40]. The signal vector \mathbf{s} can be recovered
59 from sparse samples by utilizing a norm minimization approach:

$$\min \|\mathbf{s}\|_0 \text{ subject to } \|\mathbf{y} - \Phi \mathbf{s}\|_2 < \xi \tag{2}$$

60 where ξ is measurement noise, $\|\mathbf{s}\|_0$ represents the number of nonzero entries of \mathbf{s} and
61 $\|\bullet\|_2$ is the Euclidian norm. However, it should be mentioned that it is not guaranteed
62 that eqns. (1) and (2) will provide an accurate representation of sparse signals. In some
63 applications that are sensitive to small changes such as medical diagnostic applications, it

64 is almost mandatory to achieve almost perfect recovery of these sparse signals, otherwise
65 compressive sensing schemes are not useful at all in medical diagnostic applications.
66 To reach these almost perfect reconstructions of sparse signals, compressive sensing can
67 be performed in other domains (i.e., other than the time domain), which yields a new
68 reformulation of the compressive sensing approach proposed in (1) as [64], [67]:

$$\mathbf{y} = \mathbf{\Phi}\mathbf{s} = \mathbf{\Phi}\mathbf{\Psi}\mathbf{x}. \quad (3)$$

69 Here, \mathbf{x} is the vector of expansion coefficients representing the sparse representation of
70 the signal \mathbf{s} in the basis $\mathbf{\Psi}$. A very good example of this change is representing a single
71 sinusoid in the frequency domain. This transformation would enable us to represent
72 such a sinusoid with by a two-sparse vector. In this paper, this change of the domain
73 is achieved by representing a signal in the time-frequency domain, rather than using its
74 time-domain samples.

75 It should be understood that the compressive sensing approach proposed by eqn. (3)
76 affects the sparsity in the transform domain, which then inherently affects the number
77 of measurements needed to reconstruct a signal. This is assessed using the so-called
78 coherence measure between the matrices $\mathbf{\Phi}$ and $\mathbf{\Psi}$ [70], [71], [72], [73]:

$$\mu(\mathbf{\Phi}, \mathbf{\Psi}) = \sqrt{N} \max |\langle \phi_k, \psi_j \rangle| \quad (4)$$

79 where N is the signal length, ϕ_k is the k^{th} row of $\mathbf{\Phi}$, and ψ_j is the j^{th} row of $\mathbf{\Psi}$. Smaller
80 values of the coherence measure typically denote that a smaller number of random mea-
81 surements is needed to accurately reconstruct a signal.

82 3. Time-frequency based compressive sensing

83 The time-frequency domain represent an ideal domain to sparsely represent nonsta-
84 tionary signals for several different reasons. First, it is very difficult to represent nonsta-
85 tionary signals sparsely either in time or frequency domains. For example, a frequency
86 modulated signal is concentrated along its instantaneous frequency in the time-frequency
87 domain, and most of other values are equal to zero. But, its frequency domain repre-
88 sentation has many non-zero components, and its time domain representation typically
89 has many (large) amplitude changes that can be difficult to compress. Therefore, such a

90 frequency modulated signal or any other signal with complex non-stationary structures
 91 should be compressively sampled in the time-frequency domain, as their representations
 92 are often sparse in the time-frequency domain [74], [75], [76]. Second, recent advances in
 93 computational resources enabled fast manipulations of large matrices, which are required
 94 for compressive sensing of nonstationary signals in the time-frequency domain [77].

95 In this section, we will overview two major approaches for compressive sensing of
 96 nonstationary signals in the time-frequency domain. We will begin with compressively
 97 sampling a nonstationary signal in the ambiguity domain as proposed in [78] with un-
 98 derstanding that this approach is only applicable for quadratic time-frequency represen-
 99 tations. A more general approach is to utilize time-frequency dictionaries to obtain a
 100 sparse time-frequency representation of a nonstationary signal, which can be then used
 101 to compressively sensed such a signal.

102 3.1. Compressive sensing in the ambiguity domain

103 As mentioned in the previous paragraph, the ambiguity domain provides a suitable
 104 framework to compressively sampled non-stationary signals. To achieve representations
 105 in the ambiguity domain, we can start with the Wigner-Ville distribution, $WVD(t, f)$,
 106 and take the two-dimensional Fourier transform of it to obtain the ambiguity domain
 107 representation [1], [79]:

$$A_x(\nu, \tau) = \mathcal{F}_{2D}\{WVD(t, f)\} \quad (5)$$

108 where \mathcal{F}_{2D} is the forward and inverse two-dimensional Fourier operator. The ambiguity
 109 domain offers an opportunity to suppress or completely remove cross-terms, which plague
 110 the quadratic time-frequency representations, as cross-terms are typically displaced from
 111 the origin in the ambiguity domain, and the auto-terms are typically centered around the
 112 origin. Therefore, low-pass filtering by multiplying the ambiguity representation of the
 113 signal, $A_x(\nu, \tau)$, by a kernel function $k(\nu, \tau)$:

$$\mathcal{A}_x(\nu, \tau) = A_x(\nu, \tau)k(\nu, \tau). \quad (6)$$

114 However, it should be mentioned here that compressive sensing approaches here are
 115 mostly used to obtain enhanced time-frequency signal energy localization in the time-
 116 frequency domain. Specifically, we compressively sample the ambiguity domain repre-
 117 sentation of the signal in order to obtain a very sparse time-frequency domain signal

118 representation. This is achieved by solving the l_1 -norm minimization problem to obtain
 119 a sparse time-frequency distribution $\widehat{\Upsilon}_x(t, f)$:

$$\widehat{\Upsilon}_x(t, f) = \arg \min_{\Upsilon_x(t, f)} \|\Upsilon_x(t, f)\|_1 \quad (7)$$

$$F_{2D}\{\Upsilon_x(t, f)\} - \mathcal{A}_x^M = 0|_{(\nu, \tau) \in \Omega} \quad (8)$$

120 where \mathcal{A}_x^M denotes the set of samples from the ambiguity domain in the region defined by
 121 the mask $(\nu, \tau) \in \Omega$, $\Upsilon_x(t, f)$ denotes the time-frequency distribution, and $\|\cdot\|_1$ denotes
 122 the ℓ_1 norm. Noise distributions can be approximated as follows:

$$\widehat{\Upsilon}_x(t, f) = \arg \min_{\Upsilon_x(t, f)} \|\Upsilon_x(t, f)\|_1 \quad (9)$$

$$\|F_{2D}\{\Upsilon_x(t, f)\} - \mathcal{A}_x^M\|_2 \leq \epsilon|_{(\nu, \tau) \in \Omega} \quad (10)$$

123 One has to carefully select samples in the ambiguity domain via an appropriate ambiguity
 124 function masking, which is formed as a small, mostly rectangular, area around the origin
 125 in the ambiguity plane. This resembles an approach taken to achieve high-resolution
 126 time-frequency distributions [80], [81], as we design the mask to pass auto-terms, and
 127 reduce cross-terms.

128 As an illustrative example of this approach, let us consider a sinusoidally-modulated
 129 signal with additive white Gaussian noise. For illustrative purposes, the time-frequency
 130 representations in Figure 1 are of size 60×60 points. Here, we consider a very small
 131 rectangular mask of size 7×7 points in the ambiguity domain, which represents just
 132 over one percent of the total number of samples. Now, let us consider the time-frequency
 133 representations of the signal. Figure 1(a) depicts the signal in the ambiguity domain
 134 which is observed as a domain of observations. The Wigner distribution is considered as
 135 a standard time-frequency distribution that can be derived from the ambiguity function in
 136 Figure 1(a) and it is the most appropriate to the considered signal type. This standard
 137 form of the time-frequency distribution is used only for the comparison purpose and
 138 it is calculated assuming the full set of samples from the ambiguity domain is available,
 139 Figure 1(b). Lastly, the compressive sensing based sparse time-frequency representation is
 140 presented in Figure 1(c). Unlike the standard time-frequency representation that requires
 141 full set of samples, the sparse representation is calculated from a very limited number
 142 of available samples. Despite this fact, we may observe that compared to the standard

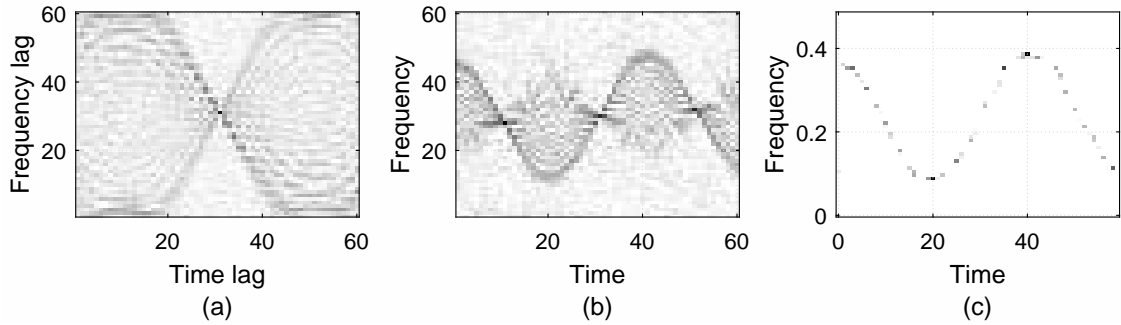


Figure 1: Representations of a sinusoidally-modulated signal in the time-frequency domain using: (a) the Wigner distributions, (b) the ambiguity function, (c) the resulting sparse time-frequency representation.

143 distribution (Figure 1(b)) the sparse representation achieved using compressive sensing
 144 approach offered a number of distinct advantages. First, it reduced the noise influence
 145 on the time-frequency representation, that is, it almost removed it completely from the
 146 distribution. Second, a number of non-zero terms in the sparse representation is about
 147 50, which represents slightly over one percent of the total number of points in the time-
 148 frequency domain. Hence, by compressively sensing the ambiguity representation of the
 149 signal, not only did we manage to compress the signal representation, but we also de-
 150 noised it.

151 An inherent issue with this approach is one requires the representation of a signal in
 152 the ambiguity domain. Hence, any hardware implementation of this approach is quite
 153 complex. Furthermore, this approach is applicable only to quadratic signal represen-
 154 tations, which limits our further signal manipulations (e.g., obtaining its time domain
 155 samples).

156 3.2. Compressive sensing based on time-frequency dictionary and matching pursuit

157 A more widely adopted approach is to utilize time-frequency dictionaries and obtain
 158 sparse signal representations using eqns. (2) and (3). Needless to say, this approach has
 159 very high computational costs which hindered its applications for many years. However,
 160 matching pursuit [82] or its variations (e.g., [83]) are very useful to avoid computational
 161 burdens associated with traditional compressive sensing approaches. Here, it is impor-
 162 tant to mention that a wide selection of time-frequency dictionaries exists, such as Gabor
 163 frames, curvelet frames, wavelet frames, overcomplete Fourier dictionaries or any combi-
 164 nations of these dictionaries [70], [84], [85], [86], [87], [88], [89], [90], [91].

Compressive sensing based implementation of a typical matching pursuit approach starts with an initial approximation of the signal, $\hat{x}^{(0)}(m) = 0$, and the residual, $R^{(0)}(m) = x(m)$. Here m represent the M time indices that are uniformly or non-uniformly distributed, that is, M time indices compressively acquired. At each subsequent stage, the matching pursuit algorithm identifies a dictionary atom with the strongest contribution to the residual and adds it to the current approximation:

$$\hat{x}^{(k)}(m) = \hat{x}^{(k-1)}(m) + \alpha_k \phi_k(m) \quad (11)$$

$$R^{(k)}(m) = x(m) - \hat{x}^{(k)}(m) \quad (12)$$

165 where $\alpha_k = \langle R^{(k-1)}(m), \phi_k(m) \rangle / \|\phi_k(m)\|^2$. The process continues till the norm of the
 166 residual $R^{(k)}(m)$ does not exceed required margin of error $\varepsilon > 0$: $\|R^{(k)}(m)\| \leq \varepsilon$ [82], or
 167 a number of bases, $\mathbf{n}_{\mathfrak{B}}$, needed for signal approximation should satisfy $\mathbf{n}_{\mathfrak{B}} \leq \mathcal{K}$. Lastly,
 168 an approximation of a compressively sampled signal is obtained using L bases as

$$x(n) = \sum_{l=1}^L \langle x(m), \phi_l(m) \rangle \phi_l(n) + R^{(L)}(n) \quad (13)$$

169 where ϕ_l are L bases from the dictionary with the strongest contributions. L bases used in
 170 the signal approximation are obtained regardless of the implemented stopping criterion.

171 The approach based on time-frequency dictionaries is suitable for any post-processing
 172 of compressively sampled signals. For example, we can easily obtain any time-frequency
 173 representation of a signal using this L -bases based approximation:

$$\mathcal{TF}\{x(n)\} = \sum_{l=1}^L \langle x(m), \phi_l(m) \rangle \mathcal{TF}\{\phi_l(n)\} \quad (14)$$

174 where $\mathcal{TF}\{\}$ is a time-frequency operator (e.g., the S-transform or short-time Fourier
 175 transform) [1], [92].

176 As mentioned in the previous paragraphs, M samples can be acquired in uniform
 177 or nonuniform manners and the exact time values are needed to acquire proper values
 178 of the time-frequency dictionary. Nevertheless, many real-life conditions may prevent
 179 us from acquiring such exact times, and there is a need to estimate the sampling time
 180 instances. This is achievable via annihilating filters contributions [38], [93], [94], which
 181 rely on determining the roots of an autoregressive filter in order to estimate the sampling
 182 instances.

183 3.2.1. A case study of a time-frequency dictionary for compressive sensing: Modulated
184 discrete prolate spheroidal sequences

185 Discrete prolate spheroidal sequences were proposed by Slepian in 1978 [95]. For
186 N samples and a normalized half-bandwidth value, W , a discrete prolate spheroidal
187 sequence, $v_k(n, N, W)$, is defined as the real solution of [95]:

$$\sum_{m=0}^{N-1} \frac{\sin[2\pi W(n-m)]}{\pi(n-m)} v_k(m, N, W) = \lambda_k(N, W) v_k(n, N, W) \quad k = 0, 1, \dots, N-1 \quad (15)$$

188 with $0 < W < 0.5$, and $\lambda_k(N, W)$ being non-zero eigenvalues of (15). The amplitude of
189 these eigenvalues can be also approximated for fixed k and large N as

$$1 - \lambda_k(N, W) \sim \frac{\sqrt{\pi}}{k!} 2^{\frac{14k+9}{4}} \alpha^{\frac{2k+1}{4}} [2 - \alpha]^{-(k+0.5)} N^{k+0.5} e^{-\gamma N} \quad (16)$$

190 where $\alpha = 1 - \cos(2\pi W)$ and $\gamma = \log \left[1 + \frac{2\sqrt{\alpha}}{\sqrt{2-\alpha}} \right]$. It can be shown that the first $2NW$
191 eigenvalues are very close to 1 while the rest rapidly decays to zero [95]. These eigenvalues
192 are also the eigenvalues of an $N \times N$ matrix $C(m, n)$ defined as [95]:

$$C(m, n) = \frac{\sin[2\pi W(n-m)]}{\pi(n-m)} \quad m, n = 0, 1, \dots, N-1. \quad (17)$$

193 By time-limiting a discrete prolate spheroidal sequence, $v_k(n, N, W)$, we can obtain an
194 eigenvector of $C(m, n)$. The discrete prolate spheroidal sequences are doubly orthogonal,
195 that is, they are orthogonal on the infinite set $\{-\infty, \dots, \infty\}$ and orthonormal on the finite
196 set $\{0, 1, \dots, N-1\}$.

197 In recent years, discrete prolate spheroidal sequences were used to obtain sparse signal
198 representations especially in the cases when these sequences and an analyzed signal are
199 in the same frequency band [96], [97]. Nevertheless, when the sequences and the signal
200 are not aligned in the frequency domain, a larger number of discrete prolate spheroidal
201 sequences is needed to obtain an accurate approximation and resulting approximations
202 are often not sparse. To avoid this issue with discrete prolate spheroidal sequences,
203 modulated discrete prolate spheroidal sequences were proposed in [96], which are defined
204 as:

$$M_k(N, W, \omega_m; n) = \exp(j\omega_m n) v_k(N, W; n) \quad (18)$$

205 where $\omega_m = 2\pi f_m$ is a modulating frequency. Modulated discrete prolate spheroidal
206 sequences are also doubly orthogonal, have most of properties of original discrete prolate

207 spheroidal sequences and are bandlimited to the frequency band $[-W + \omega_m : W + \omega_m]$
 208 [96].

Choosing a proper modulation frequency ω_m requires some a priori knowledge, or a guess. The simplest case is when a signal is confined to a known band $[\omega_1; \omega_2]$, then the modulating frequency, ω_m , and the bandwidth of the modulated discrete prolate spheroidal sequences are given by

$$\omega_m = \frac{\omega_1 + \omega_2}{2} \quad (19)$$

$$W = \left| \frac{\omega_2 - \omega_1}{2} \right| \quad (20)$$

209 as long as both satisfy:

$$|\omega_m| + W < \frac{1}{2}. \quad (21)$$

210 Nevertheless, the exact frequency band is not known in many practical applications. In
 211 general, we will only have details about a relatively wide frequency band. To account
 212 for many different possibilities, we proposed to construct a time-frequency dictionary
 213 containing bases which reflect various bandwidth scenarios [96]. This approach was used
 214 in a number of recent compressive sensing contributions [98], [92], [99], [100].

215 A sample case, depicted in Figure 2(a), involves a signal consisting of four basis func-
 216 tions from a 25-band dictionary based on modulated discrete prolate spheroidal functions
 217 with the normalized half-bandwidth equal to $W = 0.495$ and $N = 256$. For both uniform
 218 and non-uniform sampling, only 42 samples were needed to accurately recover the signal
 219 (less than 17% of the total number of samples) and its spectrograms based on regular
 220 and irregular sample times as shown in 2(c) and (d). A greater percentage of samples
 221 was required for this case in comparison to the first case as the second case is recovered
 222 almost exactly.

223 3.3. Compressive sensing in the time-frequency domain using short-time Fourier trans- 224 form sparsity

225 Many of the signals appearing in real applications have a sparse representation in the
 226 Fourier transform domain, but also in the short-time Fourier transform domain [101],
 227 [102]. However, when the signal is affected by the noise, the number of non-zero compo-
 228 nents significantly increases thus ruining the sparsity, as shown in Figure 3(a) (its sorted

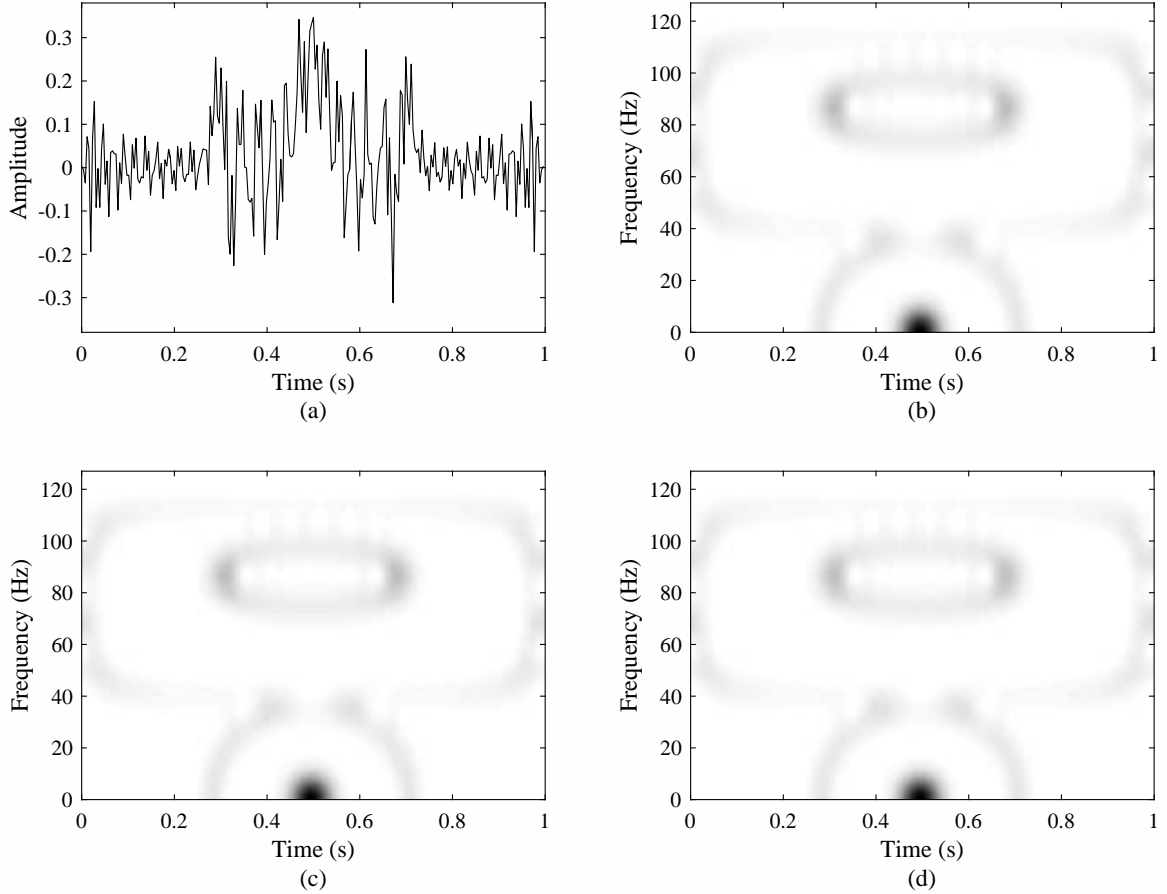


Figure 2: The time domain representation of the consider signal is shown in (a). Spectrograms of: (b) the original signal; (c) the signal based on equal distance samples; (d) the signal based on irregular samples.

229 values are shown in Figure 3(b)). By applying the L-estimation over columns of the short-
 230 time Fourier transform matrix, we may discard most of the unwanted coefficients from
 231 the short-time Fourier transform domain [103], [32]. However, many useful coefficients
 232 are also discarded in this process and we need to recover them using the compressive
 233 sensing approach. In the matrix form the short-time Fourier transform vector calculated
 234 at the time instant n using a rectangular window of size M can be defined as follow:

$$\begin{bmatrix} STFT(n, 0) \\ STFT(n, 1) \\ \vdots \\ STFT(n, M-1) \end{bmatrix} = \begin{bmatrix} \Psi(0, 0) & \dots & \Psi(0, M-1) \\ \Psi(1, 0) & \dots & \Psi(1, M-1) \\ \vdots & \dots & \vdots \\ \Psi(M-1, 0) & \dots & \Psi(M-1, M-1) \end{bmatrix} \begin{bmatrix} x(n) \\ x(n+1) \\ \vdots \\ x(n+M-1) \end{bmatrix} \quad (22)$$

235 or in a more compact form:

$$\mathbf{STFT}_M(n) = \Psi_M \mathbf{x}_M(n) \quad (23)$$

236 where Ψ_M is the discrete Fourier transform matrix of size $M \times M$:

$$\Psi(m, k) = \exp\left(-\frac{2\pi km}{M}\right) \quad m = 0, 1, \dots, M-1, k = 0, 1, \dots, M-1 \quad (24)$$

237 The index M denotes the size of corresponding vectors. For the sake of simplicity, let
 238 us assume the non-overlapping windows, meaning that the short-time Fourier transform
 239 is calculated for time instants n taken with the step $M : \{0, M, 2M, \dots, N - M\}$. The
 240 short-time Fourier transform calculation results in a set of short-time Fourier transform
 241 vectors: $\mathbf{STFT}_M(0), \mathbf{STFT}_M(M), \dots, \mathbf{STFT}_M(N - M)$. Therefore, the STFT for all
 242 considered time instants $n \in \{0, M, 2M, \dots, N - M\}$ is defined as follows [32]:

$$\begin{bmatrix} \mathbf{STFT}_M(0) \\ \mathbf{STFT}_M(M) \\ \vdots \\ \mathbf{STFT}_M(N - M) \end{bmatrix} = \begin{bmatrix} \Psi_M & \dots & 0_M \\ 0_M & \dots & 0_M \\ \vdots & \dots & \vdots \\ 0_M & \dots & \Psi_M \end{bmatrix} \begin{bmatrix} \mathbf{x}_M(0) \\ \mathbf{x}_M(M) \\ \vdots \\ \mathbf{x}_M(N - M) \end{bmatrix} \quad (25)$$

243 or equivalently: $STFT = \Theta \mathbf{x}$. The signal vector \mathbf{x} consists of N samples and can be
 244 expressed using a sparse vector \mathbf{X} of DFT coefficients:

$$\mathbf{x} = \Psi_N^{-1} \mathbf{X} \quad (26)$$

245 where Ψ_N^{-1} is the N -point inverse Fourier transform. Hence, the relationship between
 246 the short-time Fourier transform and discrete Fourier transform vectors can be written
 247 as follows:

$$\mathbf{STFT} = (\Theta \Psi_N^{-1}) \mathbf{X} = \mathbf{A} \mathbf{X}. \quad (27)$$

248 Now, let assume that the short-time Fourier transform is subject to L-estimation based
 249 filtering. After sorting the values of \mathbf{STFT} and discarding a certain percent of the
 250 highest and the lowest components, we are left with missing data in the short-time Fourier
 251 transform domain. On the positions of discarded components, the zero values remain
 252 (Figure 3(c)). Hence, a compressive sensing problem can be observed in the short-time
 253 Fourier transform domain:

$$\mathbf{y} = \mathbf{A}_{cs} \mathbf{X}. \quad (28)$$

254 where

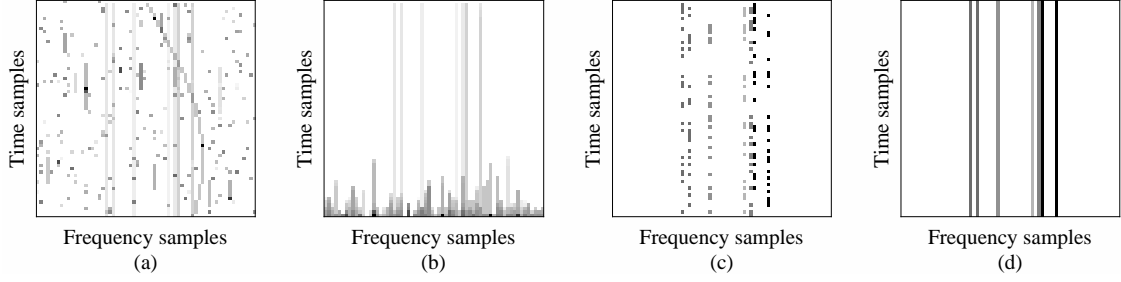


Figure 3: Compressive sensing and short-time Fourier transform: (a) noisy short-time Fourier transform; (b) sorted values of the noisy short-time Fourier transform; (c) available samples in the short-time Fourier transform after L-estimation; (d) reconstructed stationary components.

- 255 • \mathbf{y} is a vector of N_a available values from **STFT** (i.e., nonzero values);
- 256 • \mathbf{X} is a sparse discrete Fourier transform vector;
- 257 • \mathbf{A}_{cs} is obtained from $(\Theta\Psi_N^{-1})$ after removing the rows on the positions of missing
- 258 samples in **STFT**.

259 In order to reconstruct **STFT**, the minimization problem is observed in the form:

$$\min\|\mathbf{X}\|_1 \text{ s.t. } \mathbf{y} = \mathbf{A}_{cs}\mathbf{X}. \quad (29)$$

260 The reconstructed stationary components in the short-time Fourier transform domain are
 261 shown in Figure 3(d).

262 The amplitudes of the reconstructed components in the DFT domain corresponds
 263 to the original signal components: [2, 2, 1.5, 1, 1.7, 3.5, 3.5]. The proposed method is
 264 compared with the results produced by an ideal case of notch filter (its inverse form),
 265 where we need to assume that all signal frequencies are known. The ideal notch filter
 266 response will pick all values along the considered frequencies, meaning that will pick
 267 also the noise producing wrong amplitudes of certain signal components as follows. The
 268 recovered amplitudes of components are as follows: [2, 2, 1.5, 1.14, 2.17, 3.6, 3.76] as
 269 shown in Figure 4.

270 Finally, let us consider a real-world radar signal. The radar signal consist of five
 271 rigid body components (stationary components) and three corner reflectors rotating at
 272 60 RPM (nonstationary components). The stationary and non-stationary components
 273 intersects in both time and frequency dimensions. The short-time Fourier transformation

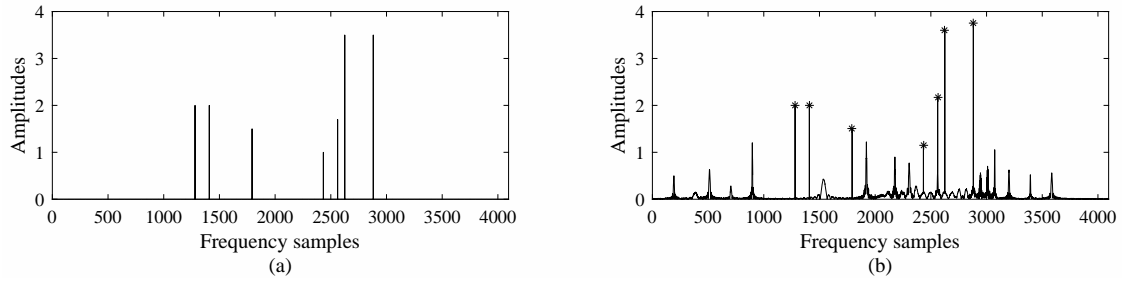


Figure 4: Comparing time-frequency based compressive sensing approaches and a notch filter: (a) reconstructed frequency components obtained using the proposed approach; (b) noisy components that would be selected by an ideal notch filter are marked by '*'.

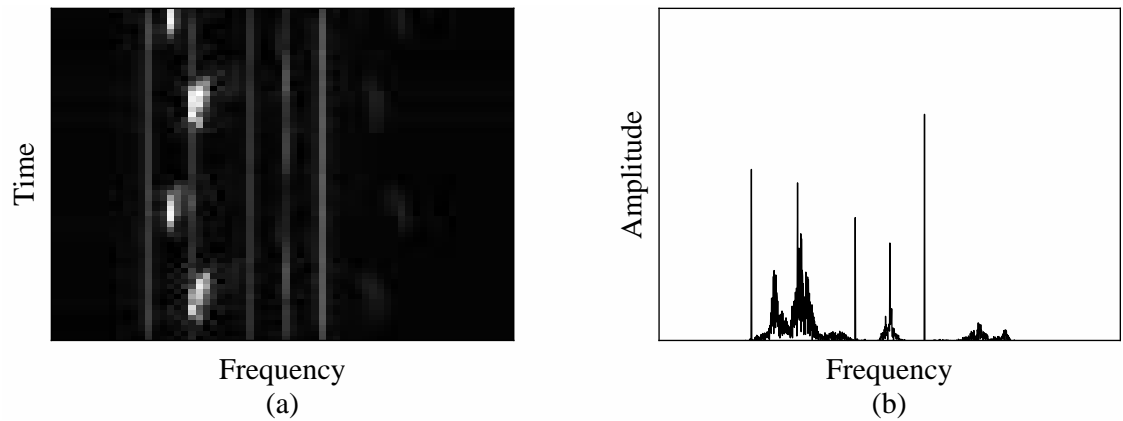


Figure 5: A sample radar signal: (a) the short-time Fourier transform of the observed signal; (b) the corresponding Fourier transform.

274 of the observed signal is shown in Figure 5(a), while the Fourier transform of the signal
 275 is shown in Figure 5(b).

276 The goal is to separate the micro-Doppler and rigid body components. As previously
 277 described, the short-time Fourier transform is calculated using non-overlapping windows
 278 (Figure 6(a)). The values in the short-time Fourier transform matrix are then sorted and
 279 50% of lowest values are discarded. Namely, the micro-Doppler components appears to be
 280 smaller valued than the rigid body components in the sorted time-frequency signal repre-
 281 sentation because of their shorter duration. The remaining short-time Fourier transform
 282 values are shown in Figure 6(b) and represent the compressive sensing measurements
 283 that are subject to the compressive sensing reconstruction procedure. The reconstructed
 284 stationary rigid body components are shown in Figure 6(c), while the remaining micro-
 285 Doppler components are shown in Figure 6(d).

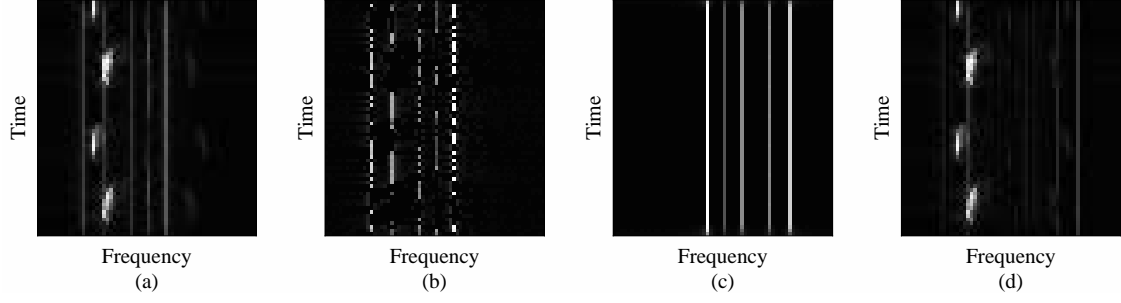


Figure 6: Compressive sensing and the short-time Fourier transform: (a) the short-time Fourier transform of the signal; (b) available samples in the short-time Fourier transform after L-estimation; (c) extracted rigid body components; (d) extracted micro-Doppler components.

3.4. Compressive sensing of signals based on the polynomial Fourier transform

The sparse representation of polynomial phase signals can be achieved by applying the polynomial Fourier transform [104]. The polynomial Fourier transform of signals $s(n)$ can be defined as follows:

$$X(k_1, \dots, k_L) = \sum_{n=0}^{N-1} s(n) \exp \left\{ -j \frac{2\pi}{N} \left(\frac{n^2 k_2}{2} + \dots + \frac{n^L k_L}{L!} \right) - j \frac{2\pi}{N} n k_1 \right\} \quad (30)$$

where the polynomial coefficients are assumed to be bounded integers. If $s(n)$ is a monocomponent polynomial phase signal of the form:

$$s(n) = A \exp \left\{ j \frac{2\pi}{N} \left(n \varphi_1 \frac{n^2 \varphi_2}{2} + \dots + \frac{n^L \varphi_L}{L!} \right) \right\} \quad (31)$$

and if a set of polynomial Fourier transform coefficients (k_2, k_3, \dots, k_L) match the signal phase parameters $(\varphi_2, \varphi_3, \dots, \varphi_L)$:

$$k_2 = \varphi_2, k_3 = \varphi_3, \dots, k_L = \varphi_L \quad (32)$$

then we will obtain the sinusoid in the polynomial Fourier transform domain at the position $k_1 = \varphi_1$. Otherwise, the polynomial Fourier transform of $s(n)$ is not sparse. In that sense, the polynomial Fourier transform can be observed as the discrete Fourier transform of $s(n)$ demodulated by the exponential term $d(n)$:

$$X(k_1, \dots, k_L) = \sum_{n=0}^{N-1} s(n) d(n) \exp \left\{ -j \frac{2\pi}{N} n k_1 \right\} \quad (33)$$

where

$$d(n) = \exp \left\{ -j \frac{2\pi}{N} \left(\frac{n^2 k_2}{2} + \dots + \frac{n^L k_L}{L!} \right) \right\} \quad (34)$$

299 The situation becomes more complex when $s(n)$ is a K -component polynomial phase
 300 signal:

$$s_K(n) = \sum_{i=1}^K A_i \exp \left\{ j \frac{2\pi}{N} \left(na_{1i} + \frac{n^2 a_{2i}}{2} + \dots + \frac{n^L a_{Li}}{L!} \right) \right\}. \quad (35)$$

301 The coefficients of demodulation term $d(n)$ should be then chosen to correspond to one
 302 of the components:

$$k_2 = \varphi_{i2}, k_3 = \varphi_{i3}, \dots, k_L = \varphi_{iL}. \quad (36)$$

303 As a result, the i th signal component is demodulated and becomes a sinusoid in the
 304 polynomial Fourier transform domain [105]. The polynomial Fourier transform represen-
 305 tation is not strictly sparse as in the case of a single polynomial phase signal, but the
 306 i th component will be dominant in the polynomial Fourier transform spectrum. In that
 307 sense, we might say that if $k_2 = \varphi_{i2}, k_3 = \varphi_{i3}, \dots, k_L = \varphi_{iL}$ is satisfied, then the poly-
 308 nomial Fourier transform is compressible with the dominant i th component. Note that the
 309 sparsity (compressibility) in the polynomial Fourier transform domain is observed with
 310 respect to the single demodulated component. Thus, we need to change the values of
 311 polynomial Fourier transform coefficients k_2, k_3, k_L within a certain range $[k_{min}, k_{max}]$ un-
 312 til we obtain a dominant component in the polynomial Fourier transform domain, which
 313 means that we revealed one of the K signal components: $k_2 = \varphi_{i2}, k_3 = \varphi_{i3}, \dots, k_L = \varphi_{iL}$,
 314 $i \in [1, K]$.

315 In the compressive sensing context, the signal vector \mathbf{s} is randomly undersampled
 316 having only $N_a \ll N$ available samples. It means that the demodulation vector \mathbf{d} should
 317 be also calculated only for N_a available instants. Now, the measurement vector \mathbf{y} can be
 318 defined as follows [105]:

$$\mathbf{y} = \mathbf{s}(n_a) \mathbf{d}(n_a) = \mathbf{x}(n_a) \quad (37)$$

319 where n_a denotes available sample positions.

320 The vector form of the polynomial Fourier transform definition given by eqn. (33) is
 321 given by:

$$\mathbf{X} = \Psi_N \mathbf{x} \quad (38)$$

322 where Ψ_N^N is a $N \times N$ discrete Fourier transform matrix. From eqns. (37) and (38), we
 323 may write:

$$\mathbf{y} = \Psi_{N_a}^{-1} \mathbf{X} \quad (39)$$

Algorithm 1 Calculate compressive sensing based polynomial Fourier transform

Require: $n_a > 0$

```

for  $k_j = k_{min} : \text{step} : k_{max}, j = 2, \dots, L$  do
   $\mathbf{y} = \mathbf{s}(n_a)\mathbf{d}(n_a)$ 
   $\mathbf{X} = \Psi_{N_a}\mathbf{y}$ 
  if  $k_2 = \varphi_{i2}, k_3 = \varphi_{i3}, \dots, k_L = \varphi_{iL} \Leftrightarrow$  there is a dominant sinusoid  $\mathbf{X}_i$  then
     $k_{1i} = \arg \max(\mathbf{X})$ 
    Save  $\mathbf{k}_i = (k_1, k_2, \dots, k_L) = (\varphi_{1i}, \varphi_{2i}, \dots, \varphi_{Li})$ 
  end if
end for

```

324 where $\Psi_{N_a}^{-1}$ is the partial random inverse Fourier matrix of size $N_a \times N$ obtained by
 325 omitting rows from inverse discrete Fourier transform matrix $\Psi_{N_a}^{-1}$ that correspond to
 326 the unavailable samples. If the demodulation term is chosen such that $k_2 = \varphi_{i2}, k_3 =$
 327 $\varphi_{i3}, \dots, k_L = \varphi_{iL}$ then \mathbf{X} can be observed as a demodulated version of the i th signal
 328 component \mathbf{X}_i , having the dominant i th component in the spectrum with the support
 329 k_{1i} . Other components in spectrum are much lower than \mathbf{X}_i and could be observed as
 330 noise. The minimization problem can be written in the form:

$$\min \|\mathbf{X}_i\|_1 \text{ subject to } \|\mathbf{y}\Psi_{N_a}^{-1}\mathbf{X}\|_2 < \xi. \quad (40)$$

331 The procedure can be described in the form of pseudo code as shown in Algorithm 1.
 332 Hence, as a result of this phase we have identified the sets of signal phase parameters:
 333 $\mathbf{k}_i = (k_1, k_2, \dots, k_L) = (\varphi_{1i}, \varphi_{2i}, \dots, \varphi_{Li})$.

334 Next, we need to recover the exact components amplitudes. Denote the set of available
 335 signal samples positions by $\mathbf{n}_a = (n_1, n_2, \dots, n_{N_a})$. In order to calculate the exact amplitudes
 336 A_1, A_2, \dots, A_K of K signal components, we observe the set of equations in the form:

$$\begin{bmatrix} s(n_1) \\ s(n_2) \\ \vdots \\ s(n_{N_a}) \end{bmatrix} = \begin{bmatrix} \Phi(1, 1) & \dots & \Phi(1, K) \\ \Phi(2, 1) & \dots & \Phi(2, K) \\ \vdots & \dots & \vdots \\ \Phi(N_a, 1) & \dots & \Phi(N_a, K) \end{bmatrix} \begin{bmatrix} A_1 \\ A_2 \\ \vdots \\ A_K \end{bmatrix} \quad (41)$$

337 where

$$\Phi(j, i) = \exp \left\{ j \frac{2\pi}{N} (n_j k_{1i} + \dots + n_j^L k_{Li}) \right\} \quad j = 1, \dots, N_a; i = 1, \dots, K. \quad (42)$$

338 In other words we have another system of equations given by:

$$\mathbf{s}(n_a) = \mathbf{\Phi}\alpha \quad (43)$$

339 where $\alpha = [A_1, \dots, A_K]^T$ contains the desired K signal amplitudes. The rows of $\mathbf{\Phi}$ cor-
 340 respond to positions of measurements n_1, n_2, \dots, n_{N_a} , and columns correspond to the K
 341 components with phase parameters $(k_1, k_2, \dots, k_L) = (\varphi_{1i}, \varphi_{2i}, \dots, \varphi_{Li})$, for $i = 1, \dots, K$.
 342 The solution of the observed problem can be obtained in the least square sense as:

$$\alpha = (\mathbf{\Phi}^* \mathbf{\Phi})^{-1} \mathbf{\Phi}^* \sim(n_a) \quad (44)$$

343 Let us consider a polynomial phase signal in the form that consists of three chirp com-
 344 ponents:

$$\begin{aligned} s(t) &= s_1(t) + s_2(t) + s_3(t) \\ &= \exp(-j\pi\varphi_{21}t^2 + j\pi\varphi_{11}t) + \exp(-j\pi\varphi_{22}t^2 + j\pi\varphi_{12}t) + \exp(-j\pi\varphi_{23}t^2 + j\pi\varphi_{13}t) \\ &= \exp(-j\pi 8Tt^2 + j\pi 16Tt) + \exp(-j\pi 32Tt^2 + j\pi 16Tt) + \exp(-j\pi 8Tt^2 + j\pi 16Tt) \end{aligned}$$

345 where the signal parameters are given as: $t = [-1/2, 1/2)$ with step $\Delta t = 1/1024$, $T = 32$,
 346 and the total signal length is 1024 samples. Observe that there are three chirp components
 347 with the rates: $\varphi_{21} = 8T$, $\varphi_{22} = 32T$, $\varphi_{23} = 8T$. The demodulation term is given in the
 348 form $d(t) = \exp(j2\pi k_2 T t^2)$. We need to search for parameter k_2 . Thus, we change the
 349 values of parameter k_2 within a predefined range to match components one after the
 350 other. The discrete Fourier transform spectrum of full length signal before applying the
 351 demodulation term (as a part of the polynomial Fourier transform) is shown in Figure
 352 7(a). When $k_2 = -8T$, the first component is detected and it becomes dominant in the
 353 spectrum (Figure 7(b)). The same situation appears when $k_2 = 32T$ (Figure 7(c)) and
 354 $k_2 = 8T$ (Figure 7(d)).

355 We may observe that the polynomial Fourier transform with an appropriate demodu-
 356 lation term $d(t)$ can be considered as compressible for the dominant component matched
 357 by the demodulation term. As such, it is amenable for compressive sensing reconstruction.

358 Next, we consider a small number of randomly selected available samples, i.e., 128 out
 359 of 1024 are available (12.5% of the total signal length). The missing samples within $s(t)$
 360 are considered as zero values, and then the demodulation term is applied iteratively for

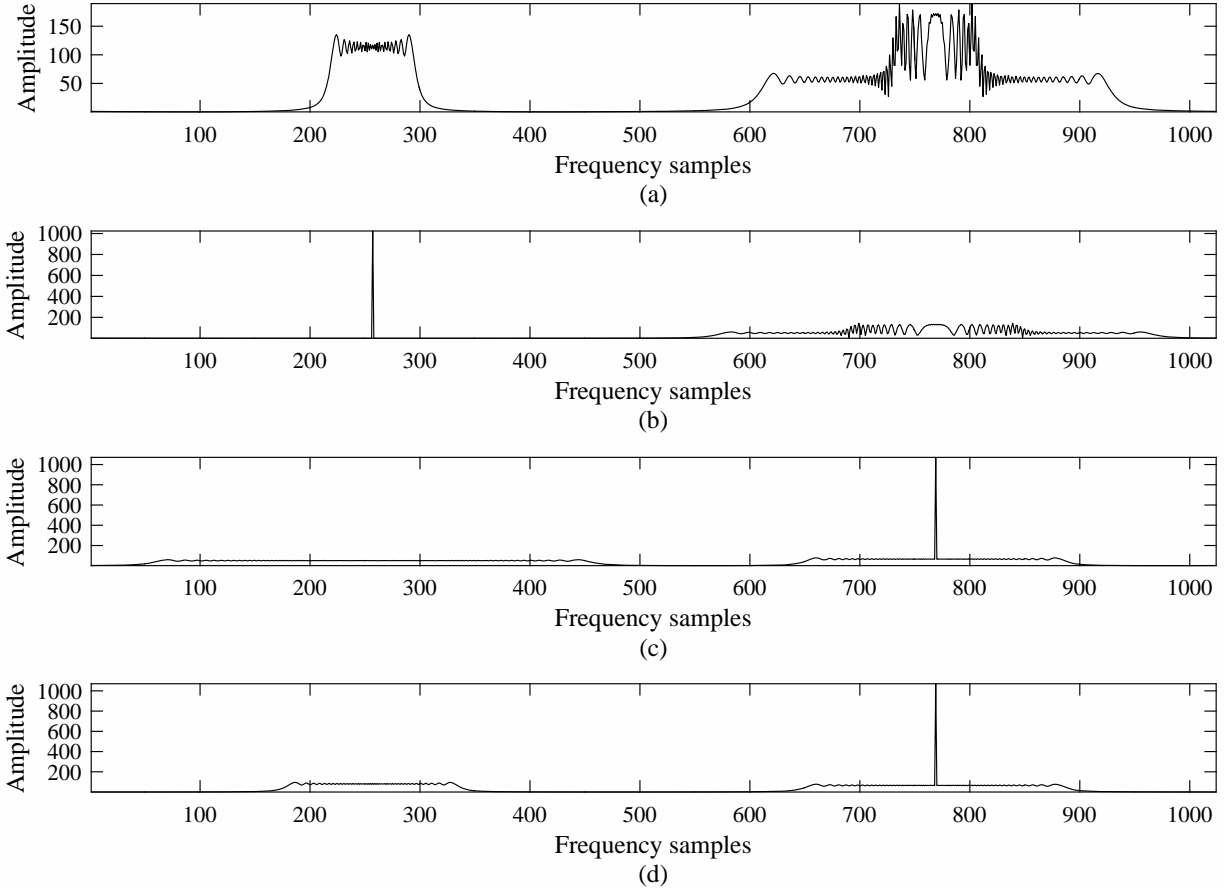


Figure 7: The effects of demodulation on the discrete Fourier transform spectrum: (a) the discrete Fourier transform of $s(t)$ before demodulation; (b) demodulation with $k_2 = -8T$; (c) demodulation with $k_2 = 32T$; (d) demodulation with $k_2 = 8T$.

361 a range of values k_2 . The results for the PFT when k_2 matches $\varphi_{21} = -8T$, $\varphi_{22} = 32T$
362 and $\varphi_{23} = 8T$ are given in Figures 8(a)-(c). Note that noise appears as a consequence
363 of missing samples that are set to zero value in order to calculate the initial polynomial
364 Fourier transform. However, the demodulated components are prominent in the spectrum
365 (Figure 8). For the illustration, Figure 9 depicts the initial polynomial Fourier transform
366 when k_2 does not match any of φ_{21} , φ_{22} and φ_{23} . The spectrum is noisy with no dominant
367 components revealed.

368 The compressive sensing reconstruction method needs to determine the support of
369 components revealed after the appropriate demodulation as shown in Figure 8. In the
370 same time, it should ignore the cases with inappropriate k_2 . The simplest solution can
371 be achieved using a threshold derived for the single iteration compressive sensing recon-
372 struction algorithm, proposed in [106]. When the threshold (horizontal red line in Fig.

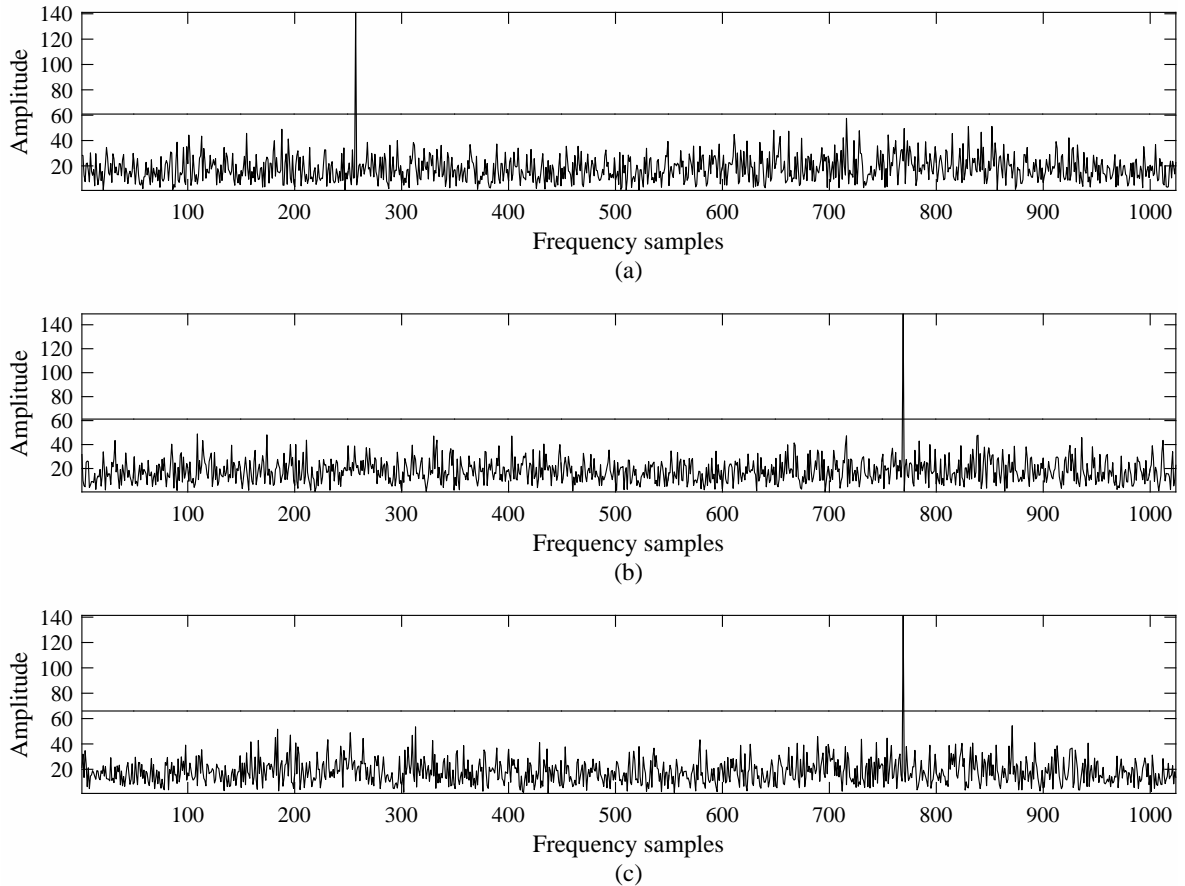


Figure 8: The polynomial Fourier transform for the compressive sensing case: (a) demodulation with $\varphi_{21} = -8T$; (b) demodulation with $\varphi_{22} = 32T$; (c) demodulation with $\varphi_{23} = 8T$.

373 3) is applied on the spectrum after demodulation with appropriate k_2 (k_2 matches either
374 $\varphi_{21} = -8T$, $\varphi_{22} = 32T$ and $\varphi_{23} = 8T$), a support of demodulated component is returned
375 as a result: $\varphi_{11} = -8T$, $\varphi_{12} = -16T$ and $\varphi_{13} = 16T$. Otherwise, when the threshold is
376 applied to the spectrum after demodulation with inappropriate (wrong k_2), the method
377 returns no support (Figure 9).

378 4. Compressive sensing based time-frequency representations

379 Most of time-frequency distributions can be observed as the Fourier transforms of
380 the local autocorrelation functions. In order to produce highly localized energy distribu-
381 tions, the autocorrelation functions must locally approximate a sinusoidal signal at each
382 time sample. The overall instantaneous frequency characteristics are obtained based on
383 the individual sinusoidal frequencies from different shifted signal windows [107], [108],

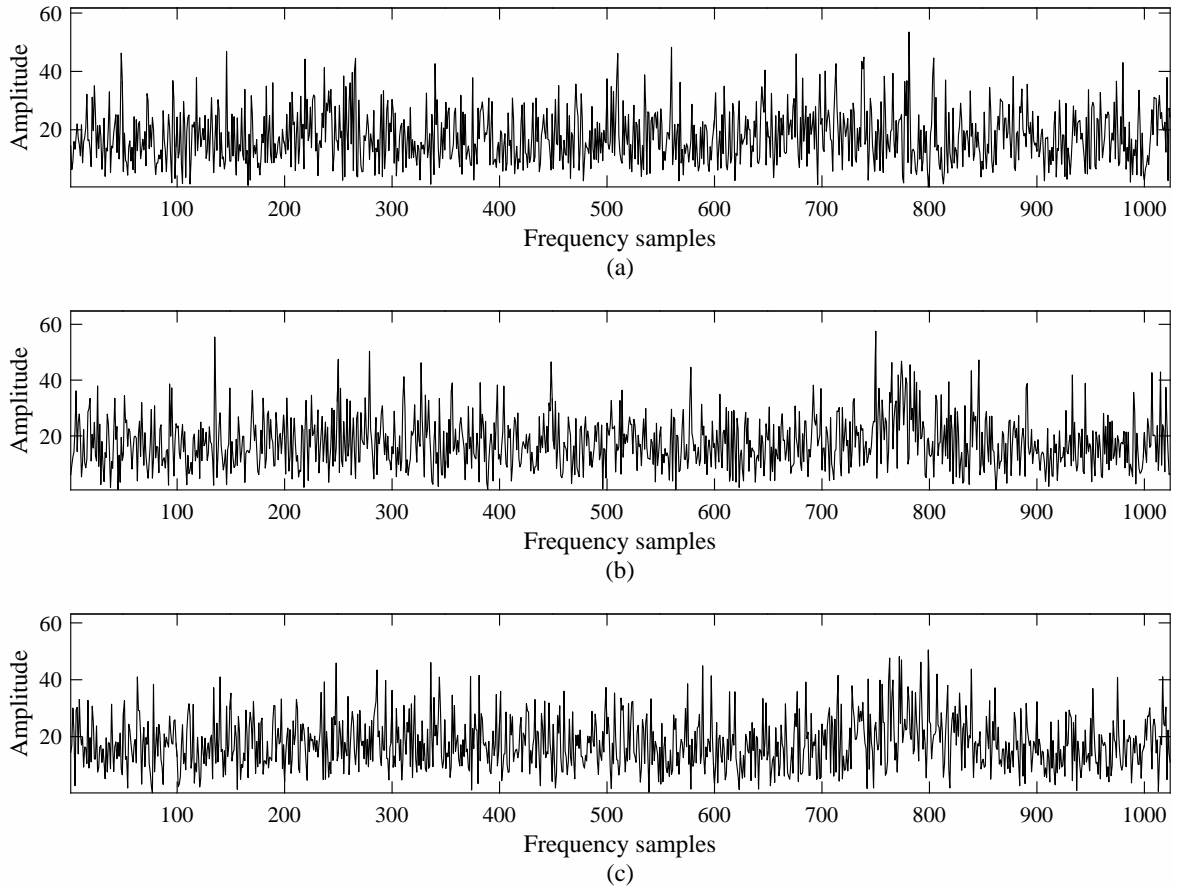


Figure 9: Compressive sensing of the polynomial Fourier transform with an incorrect demodulation term: (a) demodulation with $k_2 = 18T$; (b) demodulation with $k_2 = 12T$; (c) demodulation with $k_2 = 16T$

384 [109], [110]. In the context of compressive sensing, we observe the case when a signal
 385 is represented by a small set of random samples. Consequently, only a small percent
 386 of total autocorrelation function samples are considered as available for time-frequency
 387 distribution calculations and instantaneous frequency estimations. The standard form
 388 of time-frequency distributions calculated from coarsely under-sampled autocorrelation
 389 functions would be seriously degraded by noise, with amplitudes of components being
 390 much below their true values. As a solution, we can consider compressive sensing based
 391 time-frequency representations obtained by applying the compressive sensing reconstruc-
 392 tion algorithm to autocorrelation functions, in lieu of the Fourier transform, to achieve
 393 an ideal time-frequency signal representations [111], [112].

394 We can start with a definition of time-frequency distributions defined as the Fourier

395 transform of a higher order local autocorrelation function:

$$TFD(t, f) = \int_{-\infty}^{+\infty} R(t, \tau) e^{-j2\pi\tau} d\tau. \quad (45)$$

396 The general form of the local autocorrelation function can be defined as follows:

$$R(t, \tau) = \prod_{i=1}^{P/2} x^{b_i}(t + a_i\tau) x^{*b_i}(t - a_i\tau) \quad (46)$$

397 where P is an even number representing the order of a distribution, while the coefficients
 398 a_i and b_i depend on a particular time-frequency distribution. Without loss of generality,
 399 the rectangular window function is assumed. For instance,

- 400 1. The Wigner distribution is obtained when $P = 2$ and $a_1 = 1/2$, and $b_1 = 1$.
- 401 2. The L-Wigner distribution is obtained when $P = 2$, $a_1 = 1/(2L)$, and $b_1 = L$ as it
 402 yields $R(t, \tau) = x^L(t + \frac{\tau}{2L}) x^{*L}(t - \frac{\tau}{2L})$.
- 403 3. For $P = 4$ and $a_1 = 0.675$, $b_1 = 2$, $a_2 = -0.85$, $b_2 = 1$, the auto-correlation function
 404 in given by $R(t, \tau) = x^2(t + 0.675\tau) x^{*2}(t - 0.675\tau) x(t - 0.85\tau) x^*(t + 0.85\tau)$, which
 405 leads to the polynomial distribution.

406 Now, assume that only a small number of M random samples from $R(t, \tau)$ are available
 407 in each windowed part where $M \ll N$ holds (N is the total number of samples within
 408 the window). For the sake of simplicity we may write the autocorrelation function in the
 409 form:

$$R(t, \tau) = x_1 x_2 \dots x_p = \prod_{i=1}^P x_i \quad (47)$$

410 and

$$R(t, \tau) = \begin{cases} R(t, \tau_{n_m}) & m = 1, \dots, M \\ 0 & \text{otherwise} \end{cases} \quad (48)$$

411 where the discrete signal terms are denoted by vectors x_i , while τ_{n_m} for $m = 1, \dots, M$ are
 412 random positions of available samples in one lag-window. Hence, we have:

$$\|R(t, \tau)\|_{l_0} = \left\| \prod_{i=1}^P x_i \right\|_{l_0} = M. \quad (49)$$

413 The standard TFD calculated on the basis of $R(t, \tau)$ with missing samples, would be
 414 affected by the noise due to the missing samples. Namely, the missing samples needs to

415 be considered as zero values in $R(t, \tau)$ which will produce noise in the time-frequency
 416 domain. Hence, we consider the possibility to apply the concept of CS reconstruction
 417 in order to provide a noise-free time-frequency representation. If we observe the vec-
 418 tor of autocorrelation samples for a single time instant t_j denoted as $R(t, \tau)$, then the
 419 optimization problem can be defined as follows:

$$\min \|\mathbf{X}(t_j, \tau)\|_{l_1} \text{ subject to } R(t_j, \tau) = \mathbf{A}\mathbf{X}(t_j, f) \quad (50)$$

420 where for the observed t_j , $\mathbf{X}(t_j, f)$ represents a sparse vector belonging to an ideal time-
 421 frequency representation at the time instant t_j . The matrix \mathbf{A} is the Fourier transform
 422 based compressive sensing matrix. The minimization problem can be solved using some of
 423 the known compressive sensing reconstruction algorithms, such as the orthogonal match-
 424 ing pursuit.

425 Let us consider an illustrative example in the form:

$$x_1(t) = \exp(j160\pi t^3 - j190\pi t) \quad (51)$$

426 The polynomial distribution of the fourth order is considered for a time-frequency rep-
 427 resentation of the observed signal. The amount of available samples \mathbf{x}_1 is 35% of the
 428 total number of window samples ($N = 128$ samples). The standard polynomial distribu-
 429 tion calculated with zero values on the positions of missing samples in auto-correlation
 430 function is shown in Figure 10(a). In order to provide the compressive sensing based time-
 431 frequency representation, the orthogonal matching pursuit is applied to each windowed
 432 signal part in order to recover sparse spectrum corresponding to each particular time
 433 instant. It means that in the case of the considered monocomponent signal, a single fre-
 434 quency component is obtained for each time instant, resulting in an ideal time-frequency
 435 representation as shown in Figure 10(b).

436 Similarly, let us consider a signal with a fast varying instantaneous frequency given in
 437 the form:

$$x_2(t) = \exp(j6 \sin(2.4\pi t) + j3 \cos(1.5\pi t) - j20\pi t^2) \quad (52)$$

438 As a suitable time-frequency distribution, the complex-time distribution is usually con-
 439 sidered for fast varying instantaneous frequency estimations, since it provides significant

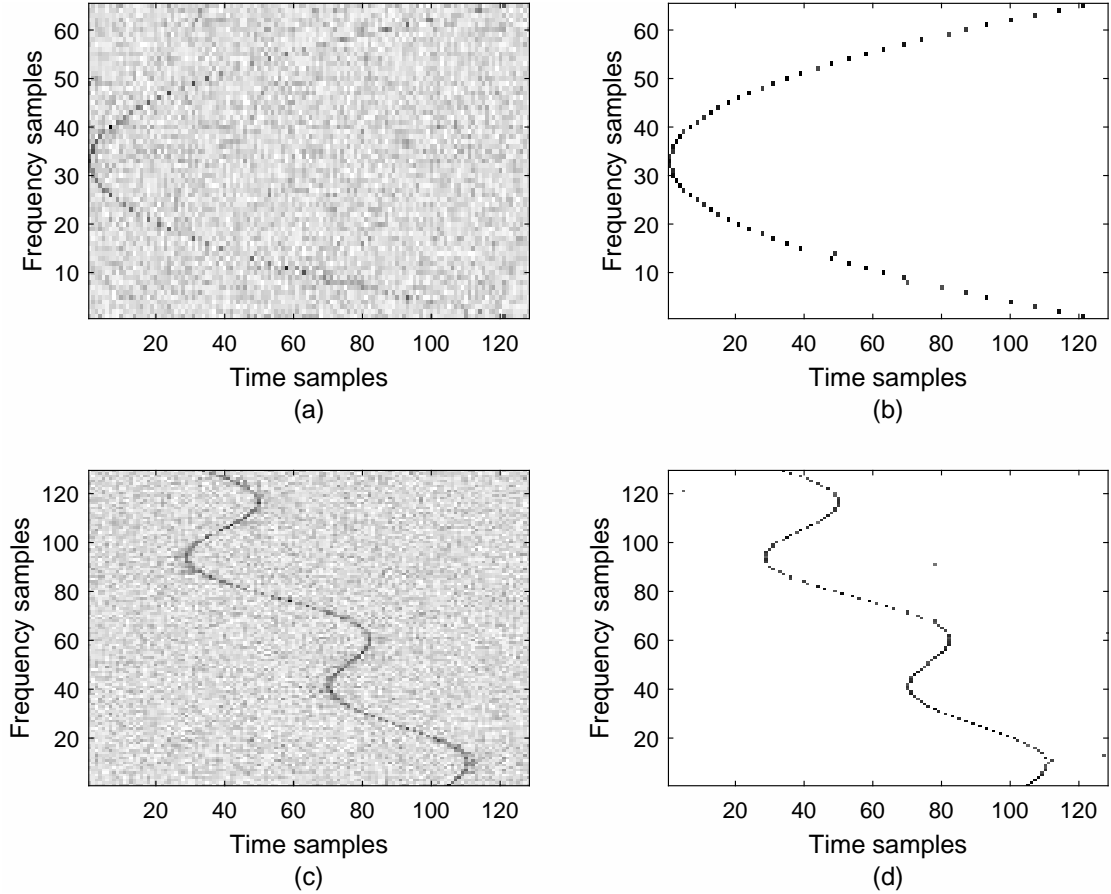


Figure 10: Comparison between the traditional time-frequency distributions and their compressive sensing based equivalents: (a) the traditional polynomial distribution $x_1(t)$, (b) a compressive sensing based polynomial distribution of $x_1(t)$ (c) the traditional complex-time distribution of $x_2(t)$, (d) a compressive sensing variant of the complex-time distribution of $x_2(t)$.

440 concentration improvements with respect to the quadratic but also polynomial distribu-
 441 tions [113], [114]. A commonly used complex-lag distribution is defined for the autocor-
 442 relation function in the form:

$$R(t, \tau) = x\left(t + \frac{\tau}{4}\right) x^{-1}\left(t - \frac{\tau}{4}\right) x^{-j}\left(t + j\frac{\tau}{4}\right) x^j\left(t - j\frac{\tau}{4}\right) \quad (53)$$

443 Let us assume that for \mathbf{x}_2 , there is approximately 40% of available samples. The stan-
 444 dard form of the complex-time distributions and its improved compressive sensing version
 445 are provided in Figures 10(c) and 10(d). The compressive sensing based complex-time
 446 distribution provides almost an ideal representation for the instantaneous frequency esti-
 447 mation. Compared to the standard form, the compressive sensing based form is noiseless
 448 and highly compressible providing a set of enhanced peaks along the instantaneous fre-

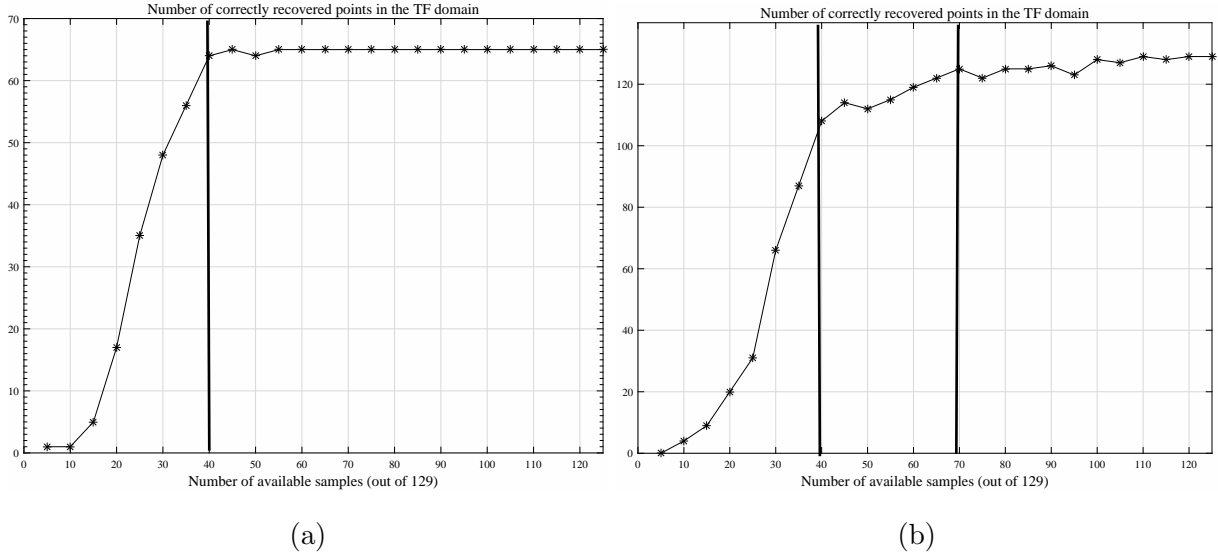


Figure 11: Estimated numbers of points to accurately estimate instantaneous frequency with (a) the polynomial distribution; (b) the complex-time distribution.

449 quency, while the other values in the tim-frequency plane are zeros.

450 Next, we estimated the required number of available samples that can provide an
 451 accurate instantaneous frequency representation after the reconstruction in the time-
 452 frequency domain. The results are shown in Figures 11a and 11b for the polynomial
 453 distribution and the complex-time distribution, respectively. The assumed signal length
 454 is 129 samples. In the case of the polynomial distribution, a high level of precision
 455 (100% of points are exactly reconstructed) is achieved with 30% of available samples
 456 (40 samples out of 129). For the complex-time distribution, we can observe that the
 457 acceptable precision is achieved even with 30% of available samples (app. 40 samples out
 458 of 129), while in the case when the amount of available samples is 55% or more (app. 70
 459 samples or more), the accurate estimation is achieved.

460 While these illustrative examples depict that the major advantage of these approaches
 461 is the fact that we can obtain very accurate representations of non-stationary signals even
 462 a small number of samples, it needs to be pointed out that these compressive sensing based
 463 time-frequency approaches are computationally more expensive than traditional time-
 464 frequency approaches. The increased computational complexity is due to the optimization
 465 procedure implemented to recover missing samples.

466 5. Conclusions and future directions

467 In this review paper, we summarized recent advances regarding compressive sensing
468 and time-frequency analysis. All these recent contributions demonstrate that compres-
469 sive sensing provided a framework for sparse time-frequency processing of non-stationary
470 signals. Based on the current contributions, we anticipate the following future directions:

- 471 • There is a great need to develop hardware solutions for all these signal processing
472 schemes consider in this paper. Hardware developments are severely lagging the
473 algorithmic development, which currently leaves many questions unanswered when
474 it comes to practical applicability of these algorithms.
- 475 • Compressive sensing based time-frequency representations address a major issue
476 associated with traditional time-frequency representations, that is, the ability to
477 obtain a time-frequency representation of a signal using only a small number of ran-
478 dom samples. However, the major disadvantage of these approaches is that they are
479 much more computationally expansive than traditional time-frequency approaches.
480 Hence, future research directions include the development of computationally in-
481 expensive compressive sensing based time-frequency representations, that have the
482 computational cost of the same order as traditional time-frequency methods.
- 483 • Adaptations of these new algorithms in many different areas is still an open ques-
484 tions. While there are applications that have highly redundant information and
485 can tolerate errors (e.g., communication systems) for which compressive sensing
486 provides excellent results, there are many more that require compressive sensing to
487 provide perfect reconstruction every time (e.g., most of medical diagnostic applica-
488 tions). Hence, the time-frequency based compressive sensing approaches have the
489 largest value in these applications requiring very high accuracies, as typical com-
490 pressive sensing approaches based on random basis dictionaries are not suitable.

491 In conclusion, this paper provides a concise summary of the work in compressive sensing
492 for sparse time-frequency precessing. While the framework provides very powerful tools
493 to process sparse non-stationary signals, we strongly believe it is still in its early stages,
494 and it is expected that further research and applications of the existing schemes will grow

495 in the near future. In our companion paper [115], we describe MATLAB functions used
496 to generate figures presented in this manuscript.

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